

Hydraulic piston made from rolled sheet metal, method for its manufacture and intermediate product of the method

5 The invention relates to a hydraulic piston made from rolled sheet metal, to a method of manufacturing such a piston and to a blank forming an intermediate product of said method. Pistons of this type are used e.g. in hydraulically actuated vehicle brakes.

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Pistons of the described type have to satisfy mutually conflicting requirements: on the one hand, they are to be light so as to have a low inertia, on the other hand, they have to be stable enough to prevent radial deformation of the side wall of the piston in the event of the base of the piston being subjected to a high load, such as occurs e.g. during a powerful braking operation because of the high hydraulic pressure in the brake system. If the last condition is not met, a total loss of function of the piston may 20 occur.

Hydraulic pistons usually have the shape of a cylindrical cup with an open end. In a portion of the outer surface of the side wall adjoining the open end of the piston there is 25 often an annular groove, which is used to fasten a protective sleeve. The region of the annular groove is particularly at risk of load-induced material deformation because the wall is weakened by the groove.

30 From WO 91/12445 a piston manufactured by a drawing method is known, in which the wall thickness in the critical groove region is not smaller than the wall thickness in the other regions of the piston. Two critical regions are mentioned in WO 91/12445, namely, on the one hand, the region 35 of the groove and, on the other hand, the inner region of a spring arrangement. The stability requirements in these two regions determine the thickness of the piston wall.

From the Russian patent 2 163 987 a drawing method for piston manufacture is known, which enables a piston to be manufactured with a stable, yet thin wall. The piston is a hollow structure with an open end. Its outer wall is cylindrical in shape and has a groove for fastening a protective sleeve. The inner surface of the piston is cylindrical in a region adjoining the open end and extending in axial direction internally over the annular groove. In a further inward lying portion of the piston the inside diameter is greater than in the region adjoining the open end. Consequently, the thickness of the side wall is greater at the open end than in the vicinity of the piston head, this being beneficial in terms of the ability to withstand axial forces in the critical region of the groove. It is however complicated to manufacture such a piston having two inner surfaces of differing inside diameter and identical outside diameter, especially as the inner surface with the smaller inside diameter lies at the open end of the piston.

The underlying object of the invention is to provide a hydraulic piston, which combines high stability with a low weight and at the open end has a wall thickness sufficient to guarantee the problem-free transmission of axial forces. The piston is moreover to be easy to manufacture. A further object is to indicate an intermediate product that arises within the framework of manufacture of the hydraulic piston.

This object is achieved according to the invention by a hydraulic piston having the features described in claim 1, by a manufacturing method comprising the steps indicated in claim 6, and by an intermediate product according to claim 16.

In contrast to cylindrical hydraulic pistons known from the prior art, the thickness of the side wall of the piston decreases monotonically from the part of the inner surface of the side wall adjoining the open end and having a cylindrical shape, to the piston head. In other words, from the cylindrically shaped portion of the inner surface of the side wall to the piston head the inside diameter of the hydraulic piston according to the invention increases monotonically. Here, by the term "monotonic" is meant, in particular, a continuous decrease of the side wall thickness and/or a continuous increase of the inside diameter. A piston thus configured presents excellent stability with regard to the required types of load and is moreover easy to manufacture.

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According to a preferred embodiment, the piston head is curved inwards, in particular in a concave manner. Such a curvature of the piston head guarantees a good ability to withstand the usual working loads.

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Preferably, when the piston head is curved inwards, the radially outer part of the piston head has the shape of a truncated cone and the central or middle part of the piston head has the shape of a spherical cap. The extension of the truncated-cone-shaped part of the piston head along its profile is in said case preferably not greater than three times the wall thickness of the side wall in its portion adjoining the piston head. A partly truncated-cone-shaped, partly spherical-cap-shaped configuration of the piston head is particularly advantageous for the shaping, by stamping, of the outer surface of the side wall in the region of transition of the side wall to the piston head.

The manufacturing method according to the invention, in its simplest form of implementation, comprises the steps of

punching a disk-shaped round blank out of a piece of rolled sheet metal, deep-drawing the disk-shaped round blank into a cup shape by means of a bottom die and a punch, stamping the cup-shaped blank to form the piston head and the cylindrical outer surface of the hydraulic piston, and incorporating an annular groove into the outer surface of the hydraulic piston. It is apparent that the manufacturing method according to the invention entails only very little cutting, e.g. for producing the annular groove. In principle, the piston is however manufactured from a rolled sheet metal by drawing and stamping operations.

In preferred developments of the manufacturing method according to the invention, the deep-drawing is effected in a plurality of steps. According to an embodiment, the disk-shaped round blank is pressed firstly by means of a first punch through a first circular die opening and then by means of a second punch through a second circular die opening, the diameter of which is smaller than the diameter of the first die opening. In the first deep-drawing step a still relatively flat, cup-shaped blank is obtained, the inside diameter of which corresponds to the outside diameter of the punch used. As a result of the reshaping of material, the thickness of the sheet metal varies. After the deep-drawing step this thickness is greater at the open end than in a transition region between side wall and head since because of the drawing operation the material thickness decreases there. The wall thickness reduction from the open end to the transition region between side wall and head occurs continuously. As a result of the second deep-drawing step the cup shape becomes narrower and higher and a further reduction of the wall thickness occurs in the region of transition from the side wall to the head. The inside diameter of the cup-shaped blank after the second deep-drawing step is determined by the outside diameter of

the punch used in the second deep-drawing step. Preferably, the punches used in the first and in the second deep-drawing step are cylindrical.

- 5 According to a particularly preferred development of the method according to the invention, the cup-shaped blank is pressed by means of a third punch through a third circular die opening, the diameter of which is smaller than the diameter of the second die opening, wherein the third punch
- 10 has a first cylindrical portion emanating from its free end and adjoined by a second cylindrical portion, the diameter of which is greater than the diameter of the first cylindrical portion and smaller than the diameter of the third die opening. By means of this third deep-drawing step,
- 15 firstly, the diameter-to-height ratio of the cup-shaped blank is altered further in the direction of the desired final shape, wherein a further decrease of the wall thickness in the transition region between the side wall and the piston head occurs, and, secondly, in the vicinity of the
- 20 open end of the blank there is formed in the side wall an inner step, which is very advantageous for subsequent machining steps.

The step in the inner surface is preferably used, after
25 deep drawing into a cup shape, to form an inwardly curved piston head by means of a first stamping operation in that a step-shaped punch comes into engagement with the step in the side wall of the blank and presses the blank into a bottom forming die.

30 This first stamping operation is preferably followed by a fourth deep-drawing step, in which the cup-shaped blank is pressed once more by means of a step-shaped punch, which comes into engagement with the step in the side wall of the
35 blank, through a fourth circular die opening, the diameter

of which is smaller than the diameter of the third die opening. In this fourth drawing step the cylindrical outer surface of the side wall is formed.

- 5 According to a particularly preferred development of the method according to the invention, subsequent to forming of the cylindrical outer surface of the side wall a second stamping operation is effected by means of a bottom forming die and a step-shaped punch, which comes into engagement
- 10 with the step in the side wall of the blank, in order to form a transition region between the piston head and the side wall. In said case, the region of the bottom die touching the piston head is advantageously cap-shaped in the centre and truncated-cone-shaped at the edge.

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- Forming of the transition region between the piston head and the side wall is preferably followed by a third stamping operation by means of a bottom forming die and a, once more, step-shaped punch, which comes into engagement with
- 20 the step in the side wall of the blank, in order to lend the piston head its final configuration.

- After forming of the annular groove, at least the outer surface may be subsequently machined. The subsequent machining of the outer surface may comprise one or more steps. The subsequent machining preferably comprises at least one of the steps: grinding, coating and polishing.

- An intermediate product according to the invention, which
- 30 arises within the framework of manufacture of the hydraulic piston, is manufactured by punching a disk-shaped round blank out of a piece of rolled sheet metal, by deep-drawing the disk-shaped round blank into a cup shape using a bottom die and a punch, as well as by stamping the cup-shaped

blank to form the piston head and the cylindrical outer surface of the hydraulic piston.

Preferred embodiments of the hydraulic piston according to
5 the invention and of the method for its manufacture are de-
scribed in detail with reference to the accompanying dia-
grammatic drawings. The drawings show:

Fig. 1 a first embodiment of a hydraulic piston according
10 to the invention in longitudinal section,

Fig. 2 a deep-drawing step effected in the framework of
manufacture of the piston of Fig. 1,

15 Fig. 3 a stamping step effected in the framework of
manufacture of the piston of Fig. 1,

Fig. 4 a punching step during manufacture of the piston
20 of Fig. 13,

Fig. 5 a first deep-drawing step during manufacture of
the piston of Fig. 13,

25 Fig. 6 a second deep-drawing step during manufacture of
the piston of Fig. 13,

Fig. 7 a third deep-drawing step during manufacture of
the piston of Fig. 13,

30 Fig. 8 a first stamping step during manufacture of the
piston of Fig. 13,

Fig. 9 a fourth deep-drawing step during manufacture of
the piston of Fig. 13,

Fig. 10 a second stamping step during manufacture of the piston of Fig. 13,

5 Fig. 11 a third stamping step during manufacture of the piston of Fig. 13,

Fig. 12 an almost finished piston in longitudinal section, and

10 Fig. 13 a second embodiment of a hydraulic piston according to the invention in longitudinal section.

Fig. 1 shows a first embodiment of a hydraulic piston 10 for a hydraulic brake of a motor vehicle in longitudinal section. The piston 10 is hollow and has an open end 12. It comprises a piston head 14, which is integrally connected to a side wall 16.

20 The side wall 16 has a cylindrical outer surface 18, let into which is an annular groove 20, which is situated in an end portion of the side wall 16 adjacent to the open end 12.

25 The side wall 16 further has an inner surface 22, which is cylindrical in a region 24 adjoining the open end 12 and extending axially over the annular groove 20. From the end of this region 24 to the piston head 14 the thickness of the side wall 16 continuously decreases, while the cylindrical outer shape is retained.

30 The dimensions of the hydraulic piston 10 may be selected in accordance with the intended application. The piston 10 may be, for example, 50.5 mm high and designed for an operating pressure of at least 160 bar. The wall thicknesses 35 a, b and c are then so selected that the piston 10 particu-

larly in the region of the annular groove 20 is stable under axial loads without increasing an optimum wall thickness c , which ensures a resistance to both axial thrust forces and radial compressive forces. For the described 5 piston size, the dimension a may be e.g. 1.9 mm, the dimension b 3.9 mm and the dimension c 3 mm. Starting from the open end 12, the cylindrical region 24 of the inner surface 22 extends approximately 16 mm in axial direction. The region of the continuous wall thickness reduction then extends 10 over a total of 31 mm in axial direction.

Fig. 2 illustrates a deep-drawing step for manufacture of the piston 10. Before this deep-drawing step, a disk-shaped round blank 26 is punched out (not shown) of rolled 15 sheet metal. This blank 26 is pressed by means of a cylindrical punch 28 through a bottom die 30 having a circular die opening 32. The dimension b is defined by the clearance between the punch 28 and the bottom die 30. Fig. 2 shows, in the left half, the initial state and, in the 20 right half, the state after effecting the deep-drawing step. The decrease of the wall thickness of the side wall 16 from the open end 12 in the direction of the piston head 14 is apparent. In this state the outer surface 18 of the side wall 16 still does not have a cylindrical shape.

25 The deep-drawing step illustrated in Fig. 2 need not be effected all at once but may be divided into a plurality of deep-drawing steps. In a first deep-drawing step, then, a still relatively flat and wide cup-shaped blank 26 is first 30 produced, which in subsequent deep-drawing steps becomes progressively narrower and higher in order to come closer and closer to the ultimately desired shape.

Fig. 3 shows a subsequent stamping step, in which the now 35 cup-shaped blank 26 is pressed by means of a further punch

34 into a further bottom die 36 in order to lend the outer surface 18 the cylindrical shape and the piston head 14 an inwardly curved shape. To achieve this, the punch 34 has a concave end face and the bottom die 36 has a convex base.

5 By means of the stamping step shown in Fig. 3 the outer surface 18 and the piston head 14 are simultaneously brought into the desired shape.

Fig. 13 shows a second embodiment of a hydraulic piston 10, 10 which differs from the embodiment illustrated in Fig. 1 in that the piston head 14 in its middle region is spherical-cap-shaped and in a radially outer region is truncated-cone-shaped.

15 Figs. 4 to 11 show a method that is eminently suitable for manufacturing the piston of Fig. 13. Each of Figs. 4 to 11 shows, on the left, an initial state and, on the right, the state reached on completion of the respective machining step.

20 Fig. 4 firstly shows a punching step, in which a disk-shaped, round blank 40 is punched by means of a punch 44 and a bottom die 46 out of a rolled sheet metal 42 of the quality 08Yu and in the present case has a thickness S_0 of 25 3.6 mm and a diameter D of 124 mm.

Fig. 5 shows a first deep-drawing step, in which the disk-shaped blank 40 is pressed by means of a first punch 48 through a first circular die opening 50 of a bottom die 52 and hence formed into a cup shape. In the present case, 30 the first punch 48 has a diameter d_1 of 72 mm, while the first die opening 50 has a diameter D_1 of 80 mm. The

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outside diameter of the now cup-shaped blank 40 at its open end is therefore 80 mm and the wall thickness S_1 in the 15 region of its open end is 4 mm. As a result of the drawing operation the wall thickness decreases continuously in the direction of the head until it reaches a value S_2 of approximately 3.5 mm in the transition region between the side wall and the head.

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Fig. 6 shows a second deep-drawing step, in which the blank 40 is brought from an outside diameter of 80 mm to an outside diameter of 65 mm in that a second cylindrical punch 54 presses the cup-shaped blank 40 through a second 25 circular die opening 56 of a bottom die 58. The outside diameter d_2 of the second punch 54 is 57 mm, while the diameter D_2 of the second die opening 56 is 65 mm. By means of this deep-drawing step a cup-shaped blank 40 is obtained, which has an inside diameter of 57 mm and an 30 outside diameter that decreases from 65 mm at the open end continuously in the direction of the head. The thickness of the side wall accordingly decreases from a value S_3 of 4 mm to a value S_4 of 3.45 mm in the region of the transition between the side wall and the head.

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Fig. 7 shows a third deep-drawing step, in which the cup-shaped blank 40 is brought from an outside diameter of 65 mm to an outside diameter of 56.5 mm in that a third cylindrical punch 60 presses the blank 40 through a third 5 circular die opening 62 of a bottom die 64. The outside diameter d_3 of the third punch 60 is 48.6 mm, while the diameter D_3 of the third die opening 62 is 56.5 mm. Once more, as a result of the drawing operation the wall thickness of the side wall of the blank 40 decreases in the

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direction of its head, close to the open end of the blank 40 said wall thickness is defined by the clearance between the side wall and the bottom die 64 and has a value S_5 of 3.95 mm, while close to the head it has a value S_6 of 15 3.4 mm. As is apparent from Fig. 7, the third punch 60 comprises a first cylindrical portion, which forms its free end and has the already mentioned outside diameter d_3 of 48.6 mm, and an adjoining, second cylindrical portion having an outside diameter of 53 mm. At the end of the third 20 deep-drawing step this second, larger-diameter portion of the third punch 60 forms a step 41 (see Fig. 12) in the inner surface of the side wall of the blank 40 by reducing the thickness of the side wall close to the open end. The radial extension of the formed step is 2.2 mm.

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Fig. 8 shows a first stamping step, in the course of which the head of the blank 40 is curved inwards. For this purpose, a step-shaped punch 66 of a complementary design to the inner surface of the blank 40 presses the blank 40 into 30 a bottom forming die 68 in that the punch 66 comes into engagement with the step 41 formed in the side wall of the blank 40. The inside diameter D_4 of the forming die opening is 56.5 mm, with the result that the outside diameter of the blank 40 is not further reduced by said opening. The 35 base of the forming die opening is formed by a punch-shaped

ejector 70, of which the surface facing the blank 40 is spherical-cap-shaped. Thus, the head of the blank 40 is deformed inwards to a concavity k_1 of 8 mm. In said case, the part of the side wall adjacent to the head is drawn 5 slightly radially inwards.

Fig. 9 shows a fourth deep-drawing step, in which the outside diameter of the blank 40 is brought from 56.5 mm to 54.3 mm in that a step-shaped punch 72, which comes into 10 engagement with the step 41 formed on the inner surface of the blank 40, presses the blank 40 through a fourth circular die opening 74 of a bottom die 76. A first cylindrical portion forming the free end of the punch 72 in said case has an outside diameter d_4 of 46.4 mm, while the fourth die 15 opening 74 has a diameter D_5 of 54.3 mm. By means of this fourth deep-drawing step the outer surface of the side wall of the blank 40 is formed into a cylinder having a diameter of 54.3 mm. Because of the cylindrical portion having the diameter d_4 and forming the free end of the punch 72, the 20 inner surface of the blank 40 also remains cylindrical in this region. In the adjoining region the inside diameter of the blank 40 increases continuously as far as the head, because the wall thickness of the side wall decreases continuously.

25 Fig. 10 shows a second stamping step, in which the transition region between the side wall and the head of the blank is formed. For this purpose, a likewise step-shaped punch 78 by coming into engagement with the shoulder 41 provided 30 on the inner surface of the blank 40 presses the blank 40 into the opening of a bottom forming die 80, the base of which is formed by a punch-like ejector 82. The surface of the ejector 82 facing the blank 40 is spherical-cap-shaped in the centre and truncated-cone-shaped at the edge. In 35 said manner, the transition region between the side wall

and the head of the blank 40 is applied against the forming die opening and forms a transition radius R_1 of 2 mm. The concavity k_1 of 8 mm is retained. The inside diameter of the forming die opening is 54.3 mm, i.e. the external dimension of the blank 40 is not altered.

Fig. 11 shows a third stamping step, in which the head of the blank 40 receives its final shape. For this purpose, a step-shaped punch 84 designed for engagement with the shoulder 41 in the blank 40 presses the blank 40 into the opening of a bottom forming die 86, the base of which is formed by a punch-shaped ejector 88. By means of the ejector 88 the concavity is increased to a value k_2 of 9 mm. The spherical-cap-shaped configuration of the head of the blank in the centre, and the truncated-cone-shaped configuration of the head at the edge is in said case retained. The transition radius between the side wall and the head of the blank 40 increases to a value R_2 of 3.4 mm.

Fig. 12 shows the almost finished hydraulic piston as a blank in longitudinal section. It is possible to see the cylindrical portion 24 of the inner surface 22, the side wall thickness decreasing continuously from the portion 24 to the head 14, a central region 90 of the head 14 with a spherical-cap-shaped configuration, and a truncated-cone-shaped edge region 92 of the head 14 that extends over a distance d , which is not greater than three times the value of wall thickness of the side wall 16 in the vicinity of the head 14. Neither the inner surface 22 nor the cylindrical outer surface 18 require further machining.

To complete the hydraulic piston 10, the part of the side wall 16 forming the step or shoulder is removed (see Fig. 13) and the annular groove 20 is worked into the outer surface 18, e.g. by cutting.

Usually, at least the outer surface 18 of the hydraulic piston 10 is subsequently machined after forming the annular groove 20. The subsequent machining may comprise e.g.

- 5 a grinding operation as well as subsequent coating with a corrosion- and abrasion-resistant material. The coated outer surface 18 may then be subjected to a polishing operation.